

Discussion 6B

The following notes are useful for this discussion: [Note 9](#), [Note 10](#)

1. System Identification by Means of Least Squares

(a) Consider the scalar discrete-time system

$$x[i+1] = ax[i] + bu[i] + w[i] \quad (1)$$

Where the scalar state at timestep i is $x[i]$, the input applied at timestep i is $u[i]$ and $w[i]$ represents some (small) external disturbance that also participated at timestep i (which we cannot predict or control, it's a purely random disturbance).

Assume that you have measurements for the states $x[i]$ from $i = 0$ to ℓ and also measurements for the controls $u[i]$ from $i = 0$ to $\ell - 1$. Further assume $\ell \geq 2$.

Show that we can set up a linear system as in eq. (2) to find constants a and b . How do we solve this system?

$$\underbrace{\begin{bmatrix} x[1] \\ x[2] \\ \vdots \\ x[\ell] \end{bmatrix}}_{\vec{s}} \approx \underbrace{\begin{bmatrix} x[0] & u[0] \\ x[1] & u[1] \\ \vdots & \vdots \\ x[\ell-1] & u[\ell-1] \end{bmatrix}}_D \underbrace{\begin{bmatrix} a \\ b \end{bmatrix}}_{\vec{p}} \quad (2)$$

(b) What if there were now two distinct scalar inputs to a scalar system

$$x[i+1] = ax[i] + b_1u_1[i] + b_2u_2[i] + w[i] \quad (3)$$

and that we have measurements as before, but now also for both of the control inputs.

Set up a least-squares problem that you can solve to get an estimate of the unknown system parameters a, b_1, b_2 .

- (c) What could go wrong in the previous case? For what kind of inputs would make least-squares fail to give you the parameters you want?

- (d) Now consider the two dimensional state case with a single input.

$$\vec{x}[i+1] = \begin{bmatrix} x_1[i+1] \\ x_2[i+1] \end{bmatrix} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \vec{x}[i] + \begin{bmatrix} b_1 \\ b_2 \end{bmatrix} u[i] + \vec{w}[i] \quad (4)$$

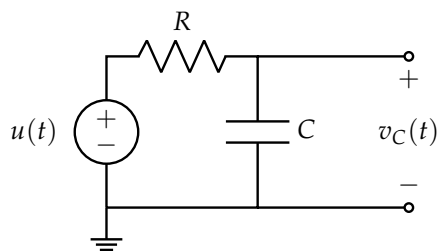
How can we treat this like two parallel problems to set this up using least-squares to get estimates for the unknown parameters $a_{11}, a_{12}, a_{21}, a_{22}, b_1, b_2$? Write the least squares solution in terms of your known matrices and vectors (including based on the labels you gave to various matrices/vectors in previous parts). *Hint: What work/computation can we reuse across the two problems?*

2. Stability Examples and Counterexamples

- (a) Consider the circuit below with $R = 1 \Omega$, $C = 0.5 F$, and $u(t)$ is some function bounded between $-K$ and K for some constant $K \in \mathbb{R}$ (for example $K \cos(t)$). Furthermore assume that $v_C(0) = 0 V$ (that the capacitor is initially discharged).

This circuit can be modeled by the differential equation

$$\frac{dv_C(t)}{dt} = -2v_C(t) + 2u(t) \quad (5)$$



Show that the differential equation is always stable (that is, as long as the input $u(t)$ is bounded, $v_C(t)$ also stays bounded). Consider what this means in the physical circuit. *HINT: You may want to use the triangle inequality, i.e. $|a + b| \leq |a| + |b|$, and the triangle inequality for integrals, i.e. $\left| \int_a^b f(x) dx \right| \leq \int_a^b |f(x)| dx$. When we use $|\cdot|$ notation here, we will take this to mean the magnitude, rather than the absolute value (since we can be dealing with complex numbers).*

- (b) **(PRACTICE)** Now, suppose that in the circuit of part 2.a we replaced the resistor with an inductor as in fig. 1.

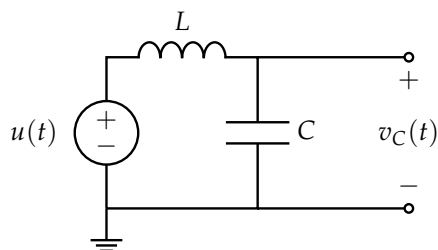


Figure 1: The original circuit with an inductor in place of the resistor.

Let $L = 1$ mH. Repeat part 2.a for the new circuit (with an inductor). Consider the following process to arrive at the result:

- i. Derive the system of differential equations using KCL, KVL, and NVA. Show that the system is $\frac{d}{dt} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{C} \\ -\frac{1}{L} & 0 \end{bmatrix} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{L} \end{bmatrix} u(t)$ with the initial condition being $\begin{bmatrix} v_C(0) \\ i_L(0) \end{bmatrix} = \vec{0}$.
- ii. Solve the matrix differential equation, using diagonalization if needed. Show that the

diagonalized system has a solution

$$\vec{y}(t) = \begin{bmatrix} \frac{1}{2LC} e^{j\frac{1}{\sqrt{LC}}t} \int_0^t e^{-j\frac{1}{\sqrt{LC}}\theta} u(\theta) d\theta \\ \frac{1}{2LC} e^{-j\frac{1}{\sqrt{LC}}t} \int_0^t e^{j\frac{1}{\sqrt{LC}}\theta} u(\theta) d\theta \end{bmatrix} \quad (6)$$

where $\vec{y}(t) = V^{-1} \begin{bmatrix} v_C(t) \\ i_L(t) \end{bmatrix}$ for change of basis matrix V . You may use the fact that the eigenvalue, eigenvector pairs of $\begin{bmatrix} 0 & \frac{1}{C} \\ -\frac{1}{L} & 0 \end{bmatrix}$ are $\left(j\frac{1}{\sqrt{LC}}, \begin{bmatrix} -j\sqrt{\frac{L}{C}} \\ 1 \end{bmatrix} \right)$ and $\left(-j\frac{1}{\sqrt{LC}}, \begin{bmatrix} j\sqrt{\frac{L}{C}} \\ 1 \end{bmatrix} \right)$.

- iii. Apply a similar process from part 2.a to show that, if we have a bounded input $u(t)$, then the system can grow unboundedly. When showing that a system is unstable, it suffices to choose a bounded $u(t)$ that makes the system unbounded. We can choose $u(t) = 2 \cos\left(\frac{1}{\sqrt{LC}}t\right) = e^{j\frac{1}{\sqrt{LC}}t} + e^{-j\frac{1}{\sqrt{LC}}t}$ ¹. HINT: You may use the fact that $i_L(t) = y_1(t) + y_2(t)$.

Hint: You might find it useful to revisit the process of generating the state-space equations for $v_C(t)$ and $i_L(t)$ as done in Note 4 for the LC Tank. The difference is that here, we have an input voltage.

- (c) Thus far, we have dealt with continuous systems so it also makes sense to consider discrete systems. Consider the discrete system

$$x[i+1] = 2x[i] + u[i] \quad (7)$$

¹The natural frequency of this system is $\omega_n = \frac{1}{\sqrt{LC}}$. If we excite this system at a period equal to the natural frequency, we can make it grow unboundedly. This is similar to pushing a swing at the same rate it swings, which makes it swing farther.

with $x[0] = 0$.

Is the system stable or unstable? If unstable, find a bounded input sequence $u[i]$ that causes the system to “blow up”.

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